

Effect of Face Mask Design and Flow-by on Rebreathing During Noninvasive Ventilation

Davide Signori, Giacomo Bellani, Serena Calcinati, Alice Grassi, Nicolò Patroniti, and Giuseppe Foti

BACKGROUND: Noninvasive ventilation (NIV) is used to treat respiratory failure because it reduces the risks of endotracheal intubation and postextubation respiratory failure. A wide range of different interfaces is available, but concerns exist about rebreathing. This study evaluated a total face mask with a 2-limb ventilation circuit and separate access for inflow and outflow gas, which was developed to reduce rebreathing. **METHODS:** In a bench test, a standard total face mask (with a single connector to the ventilation circuit) and the modified total face mask were applied to a mannequin connected to an active breathing simulator. A known CO₂ flow (\dot{V}_{CO_2}) was delivered to the mannequin's trachea. We tested the following settings: CPAP with the mechanical PEEP valve set at 8 cm H₂O (with 60 and 90 L/min continuous flow) and pressure support of 6 and 12 cm H₂O (with 2 and 15 L/min flow-by). The settings were tested at simulated breathing frequencies of 15 and 30 breaths/min and with \dot{V}_{CO_2} of 200 and 300 mL/min. The active simulator generated a tidal volume of 500 mL. Airway pressure, air flow, CO₂ concentration, and CO₂ flow as the product of air flow and CO₂ were recorded. **RESULTS:** The mean volume of CO₂ rebreathed and the minimum CO₂ inspiratory concentration were significantly lower with the modified mask than with the standard mask. The 15 L/min flow-by significantly decreased rebreathing with the DiMax0 mask, whereas it had no effect with the traditional mask. **CONCLUSIONS:** A face mask with a two-limb ventilation circuit and separate access for inflow and outflow gas reduces rebreathing during NIV. The addition of flow-by enhances this effect. Further studies are required to verify the clinical relevance. *Key words:* noninvasive ventilation; rebreathing; face mask; flow-by; bias flow; carbon dioxide clearance. [Respir Care 0;0(0):1–•. © 0 Daedalus Enterprises]

Introduction

Noninvasive ventilation (NIV) is commonly used as a first-line treatment for acute and chronic respiratory fail-

ure in certain patients (eg, COPD exacerbation, acute cardiogenic pulmonary edema).¹⁻³ NIV represents a valid strategy to reduce endotracheal intubation rates and to treat postextubation respiratory failure.⁴ Hypercapnic patients benefit considerably from NIV, which increases alveolar ventilation, decreases P_{aCO₂}, and unloads the respiratory muscles.⁵⁻⁷

However, depending on the underlying disease and disease severity, NIV failure in critically ill patients ranges

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from 5% to 60%,⁸ and interface-related problems have been identified among the possible causes of failure; air leaks, excessive pressure on the face, claustrophobia, skin lesions on the nasal bridge, facial pain, and oronasal dryness could lead to early discontinuation of NIV.⁹⁻¹¹

Some concerns have also been raised regarding the occurrence of rebreathing.¹² The relevance of rebreathing was noted in a bench study in which the rebreathed volume was as much as 55% of the tidal volume (V_T) during ventilation with a single-limb circuit and in the absence of a non-rebreathing valve.¹³ When translated to the clinical setting, the same ventilator circuit in the absence of a non-rebreathing valve led to a higher minute ventilation and work of breathing than that of a circuit with a non-rebreathing valve at the same P_{aCO_2} . Air leaks are one of the most studied NIV-related issues¹⁴: in fact, while “intentional leaks” are deliberately generated in the system to avoid rebreathing,¹⁵ “unintentional leaks” (eg, occurring between the mask and the skin, or through the mouth during nasal ventilation) can affect the effectiveness of ventilation, leading to asynchronies and NIV discontinuation.¹⁶ Therefore, a balance between modest leaks and low rebreathing has to be found, and the choice of the interface to deliver NIV is critical. In a recent trial, a helmet interface was shown to be superior to a face mask in delivering NIV to subjects with ARDS.¹⁷ The high gas flow in the helmet could contribute to reduced rebreathing; this may be one of the possible mechanisms of the findings of Patel et al.^{17,18} In fact, the use of a face mask to deliver NIV might have the drawback of increased dead space due to the inner volume of the mask and the use of a single-limb connection to the ventilator circuit shared by the inflow and outflow.^{19,20} The intermittent and limited fresh gas flow may not be enough for CO_2 clearance from inside the mask.^{12,21} One of the solutions to this problem could be the addition of a flow-by (also called bias flow, a continuous flow of gas inside the ventilatory system during the whole respiratory cycle); a flow-by, however, will only be effective in the presence of air leaks because it would otherwise circulate around the circuit Y-piece without washing out the inner mask.²²

Different types of mask were tested in a previous study to verify the effect of mask design on rebreathing. The use of a smaller mask with an exhalation port located within the mask (as opposed to a valve located on the ventilator circuit) showed the best performance.²³ However, this study was criticized because the reduction in CO_2 volume rebreathing, though statistically significant, was very small (2–3.5 mL/breath) and not clinically relevant.²⁴

In this study, we compared a new total face mask design aimed to reduce rebreathing with 2 different ports, one for the inflow fresh gas and one for the outflow exhaled gas, to a standard mask with a single gas port. We secondarily studied the effect of air leaks on rebreathing, and we tested

QUICK LOOK**Current knowledge**

Noninvasive ventilation (NIV) is commonly used to treat respiratory failure. The delivery of NIV, during both continuous-flow CPAP and pressure support ventilation, is associated with a relevant failure rate, possibly due to rebreathing, which increases the patient's respiratory load. Rebreathing is decreased by the presence of air leaks, but the interface used to deliver NIV is another determinant.

What this paper contributes to our knowledge

In a bench model, rebreathing was mitigated by a total face mask design with separate ports for inflow and outflow. The effectiveness of the new mask design in reducing rebreathing was increased in the presence of higher flow CPAP and when continuous flow-by was provided by the mechanical ventilator during NIV. In the presence of air leaks, the new face mask design was still effective in reducing rebreathing.

the effectiveness of the new mask design in the presence of leaks.

Methods**Study Protocol**

In this bench study, which was conducted in the laboratory of Dimar S.R.L. in Medolla, Italy, an active lung simulator (ASL 5000, Ingmar Medical, Pittsburgh, Pennsylvania) was connected by a tube to the mouth of a mannequin face to compare 2 total-face mask configurations (Fig. 1 illustrates the masks design and the experimental setting). The standard mask had a single connector for inflow/outflow gases (DiMax, Dimar, Medolla, Italy, inner volume 660 mL), and the modified mask had 2 different connectors for inflow and outflow gases (DiMax0, Dimar, inner volume 700 mL).

Each mask was connected to a free-flow CPAP or to an ICU ventilator (Puritan Bennett 840, Covidien) through standard circuits. A known CO_2 flow was delivered to the mannequin's trachea to simulate CO_2 production (\dot{V}_{CO_2}) of 200 mL/min or 300 mL/min (Bronkhorst High-Tech B.V., Ruurlo, The Netherlands). To avoid confounders, air loss was minimized by sealing each mask to the mannequin face with silicone for the first set of experiments. Then, to simulate a more realistic scenario similar to those found in clinical settings, some of the experiments were repeated without silicone, which allowed a leak of approximately 20% on the set V_T .

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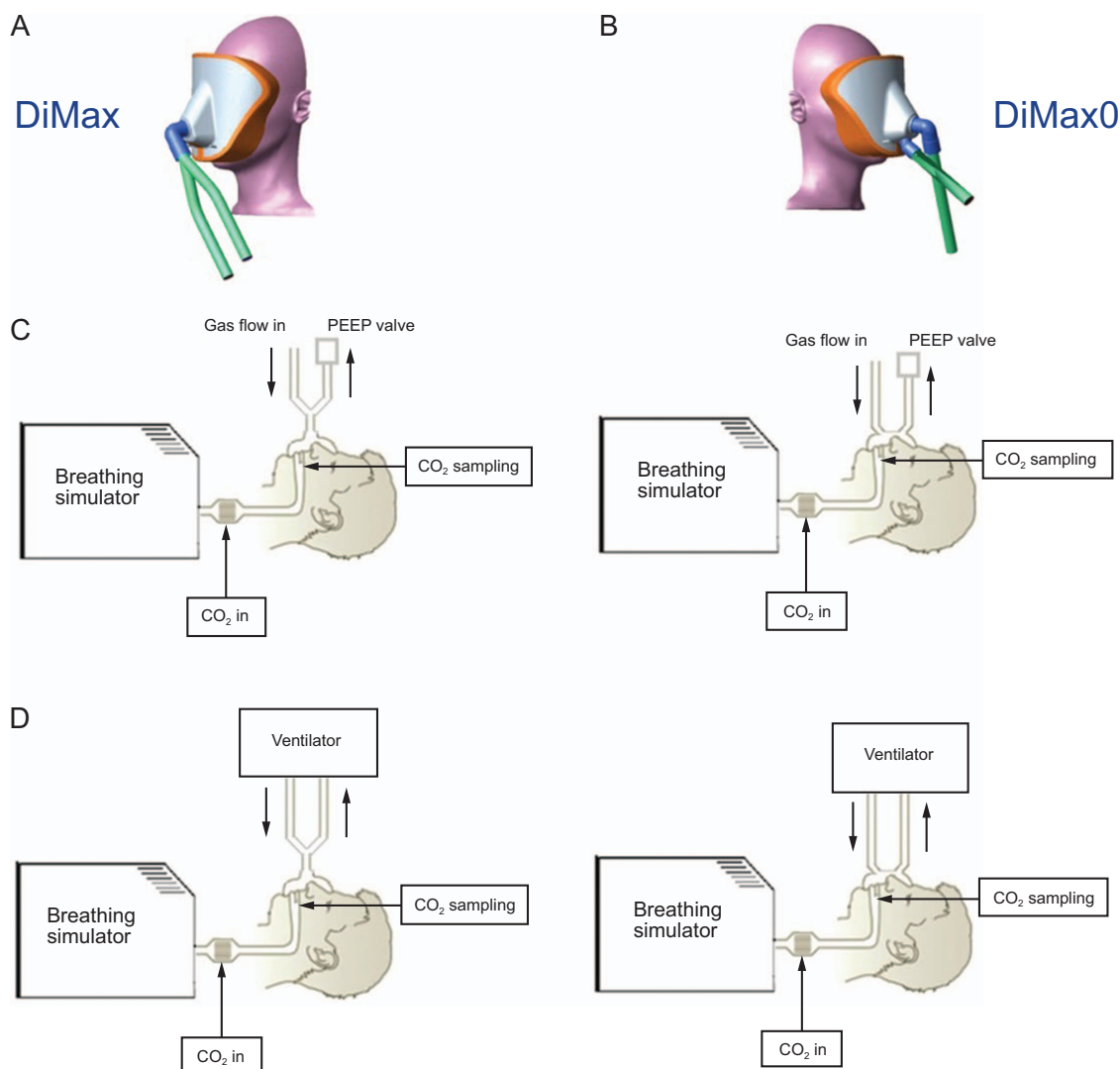


Fig. 1. Design and experimental settings for the face masks. (A) Standard mask design (DiMax). (B) Modified mask (DiMax0). (C) CPAP settings and (D) pressure support ventilation settings.

Data Acquisition

We tested 2 ventilation settings. The first was continuous-flow CPAP, which consisted of a continuous fresh gas flow of 60 L/min or 90 L/min in the tested face mask through the inspiratory branch and a mechanical PEEP valve (700/6336, Dimar) set at 8 cm H₂O on the expiratory limb. The second setting was pressure support ventilation (PSV), in which the tested face mask was connected to the ventilator (Puritan Bennet 840) by the inspiratory and expiratory limb set to deliver a pressure support of 6 cm H₂O and 12 cm H₂O, with a minimum flow-by of 2 L/min or a maximum flow-by of 15 L/min. PEEP was kept constant at 4 cm H₂O in all conditions.

Each of the aforementioned settings was tested at a simulated breathing frequency of 15 breaths/min and

30 breaths/min (see the supplementary materials at <http://www.rcjournal.com>). A negative inspiratory pressure swing of the simulator was set to generate a constant V_T of 500 mL in all conditions with an inspiratory-expiratory ratio set at 1:2. We hypothesized that the expired CO₂ through the inspiratory branch and a mechanical PEEP valve would be reduced by about 50% of the amount if the simulated breathing frequency was doubled.

Measurements

Sensors were placed at the airway opening to measure flow (SpiroQuantA+, Envitec, Lohne, Germany), pressure (First Sensor, Berlin, Germany), and mainstream CO₂ concentration (Dittrich Elektronik, Baden Baden, Germany). All of the signals were digitalized at a sampling rate of 100 Hz and recorded (Labview, National Instru-

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ments Italy, Milano, Italy). Curves were analyzed offline (Powerlab, ADInstruments, Sydney, Australia). The CO_2 flow inspired and expired by the simulator was calculated as the instantaneous product of CO_2 concentration and total airway flow. We then derived the following parameters on a breath-by-breath basis: V_T , minimum inspiratory pressure (indicator of pneumatic performance), inspired (rebreathed) CO_2 volume, and functional dead space, which indicates the amount of V_T “lost” to gas exchange due to rebreathing. The word “functional” emphasizes that this represents the fraction of V_T wasted due to rebreathing and represents the volume of gas, with a CO_2 concentration equal to the mixed expiratory CO_2 , which contains the amount of CO_2 rebreathed:

$$\text{CO}_2 \text{ rebreathed volume} / (\text{CO}_2 \text{ exhaled volume} / V_T)$$

For example, if the volume of rebreathed CO_2 were 5 mL, the volume of exhaled CO_2 were 20 mL, and the V_T were 500 mL, then the functional dead space would be 125 mL. The volume of rebreathed CO_2 is expressed as a percentage of the calculated \dot{V}_{CO_2} . Three or four breaths were needed by the simulator to adapt to ventilator settings, then a steady state was reached and the amount of rebreathing was stable in each breath, with no accumulation over time. For each condition, we sampled 30–40 breaths. Examples of the curves are reported in the data supplement (see the supplementary materials at <http://www.rcjournal.com>).

Statistical Analysis

All data are expressed as mean \pm SD. Two-way analysis of variance for repeated measures with Tukey’s post hoc analysis was used to compare airway pressure, inspired CO_2 , and rebreathed CO_2 between the 2 masks when different ventilation settings were used (CPAP with 2 different flows, PSV with or without flow-by). The same statistical test was used to compare different ventilation settings within the same mask. $P < .05$ was considered statistically significant. Statistical analysis was performed using SPSS v.24.0 (IBM, Armonk, New York).

Results

We tested the same ventilator settings with a \dot{V}_{CO_2} of 200 mL/min and 300 mL/min. All results were obtained with $\dot{V}_{\text{CO}_2} = 300$ mL/min. The results obtained with a $\dot{V}_{\text{CO}_2} = 200$ mL/min are comparable at all settings (see the supplementary materials at <http://www.rcjournal.com>).

Calculated \dot{V}_{CO_2}

The values of calculated \dot{V}_{CO_2} for the 2 masks and at the different ventilation settings are shown in the data supple-

ment (see the supplementary materials at <http://www.rcjournal.com>). The calculated \dot{V}_{CO_2} was similar to the set \dot{V}_{CO_2} (300 mL/min).

Inspiratory Pressure Drop

Minimum pressure during inspiration is shown in the data supplement (see the supplementary materials at <http://www.rcjournal.com>). This parameter allows comparison between the pneumatic performances of the 2 masks by expressing the capacity of the mask to maintain a constant pressure during the overall respiratory cycle. A pressure drop below the set level of PEEP is an indicator of poor pneumatic performance or insufficient flow. During CPAP, in both masks and with both flows and simulated breathing frequencies, the minimum inspiratory pressure was slightly lower than PEEP, with this effect being more pronounced with the simulated breathing frequency of 30 breaths/min. In PSV, the 2 masks did not show a systematic difference in pressure drop. As expected, the increase of flow-by (which also affects trigger sensitivity for the specific ventilator used) led to an increase in the inspiratory pressure drop.

Amount of Rebreathing

With continuous-flow CPAP, the DiMax0 mask reduced the amount of rebreathing in all conditions tested by about 90% with a simulated breathing frequency of 15 breaths/min and by 75% with a simulated breathing frequency of 30 breaths/min compared to the DiMax mask. At a simulated breathing frequency of 30 breaths/min, increasing the CPAP flow from 60 L/min to 90 L/min significantly reduced rebreathing within the same mask, as expected, although the effect was more pronounced with the DiMax0 mask (Fig. 2).

During PSV, at both 6 cm H_2O and 12 cm H_2O and without flow-by, the DiMax0 mask allowed a 20% reduction of rebreathing, and this benefit disappeared when the simulated breathing frequency was set at 30 breaths/min. However, the addition of a flow-by of 15 L/min was effective in reducing rebreathing with the DiMax0 mask in comparison with the DiMax mask. Again, this effect was greater at lower simulated breathing frequencies (15 breaths/min), where the DiMax0 mask reduced rebreathing by 65% versus the DiMax mask. When the simulated breathing frequency was set at 30 breaths/min, rebreathing was reduced by about 15% during PSV at both 6 cm H_2O and 12 cm H_2O (Fig. 2).

The findings were similar for the minimum concentration of CO_2 measured during inspiration (Table 1), and confirmed by the calculated differences in functional dead space (see the supplementary materials at <http://www.rcjournal.com>).

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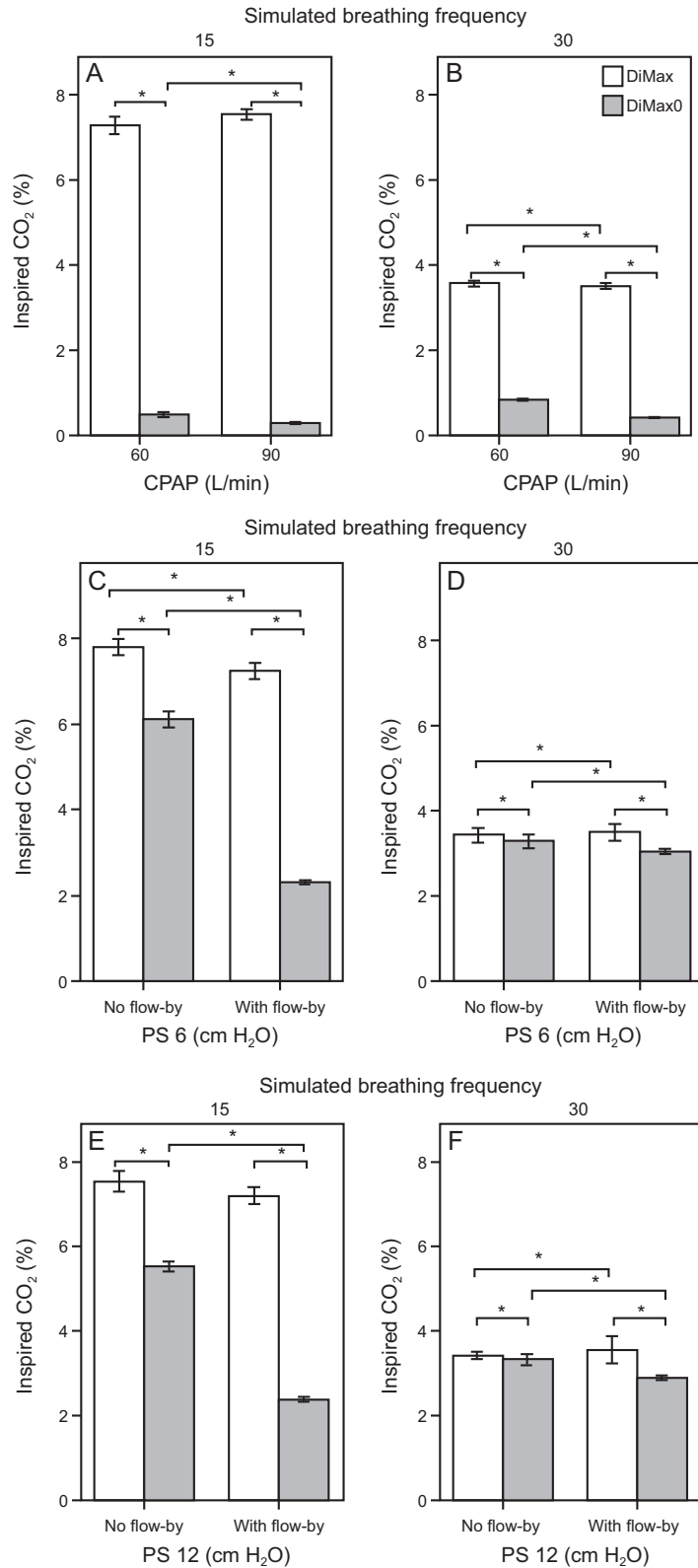


Fig. 2. Inspired CO_2 per breath, expressed as % of \dot{V}_{CO_2} : (A, B) during CPAP, (C, D) during pressure support (PS) of 6 $\text{cm H}_2\text{O} \pm$ flow-by 15 L/min, and (E, F) during PS of 12 $\text{cm H}_2\text{O} \pm$ flow-by 15 L/min. Simulated breathing frequency 15 breaths/min (A, C, and E) and 30 breaths/min (B, D, and F). Error bars indicate SD. * $P < .001$.

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Table 1. Minimum Inspiratory CO₂ Concentration Compared Between Different Face Masks and Gas Flows

Setting	Breathing Frequency, breaths/min	Minimum Inspiratory CO ₂ concentration (%), Mean (SD)				Effect of:	P
		CPAP 60 L/min or PSV Without Flow-by		CPAP 90 L/min or PSV With Flow-by			
		DiMax	DiMax0	DiMax	DiMax0		
CPAP	15	2.82 (0.12)	0.06 (0.01)	2.70 (0.17)	0.03 (0.004)	Face mask	< .001
						Gas flow	< .001
						Interaction	< .001
	30	1.37 (0.05)	0.28 (0.01)	1.39 (0.06)	0.10 (0.01)	Face mask	< .001
						Gas flow	< .001
						Interaction	< .001
PSV 6 cm H ₂ O	15	3.12 (0.14)	1.64 (0.06)	2.68 (0.14)	0.61 (0.02)	Face mask	< .001
						Flow-by	< .001
						Interaction	< .001
	30	1.43 (0.06)	1.39 (0.04)	1.47 (0.06)	0.88 (0.03)	Face mask	< .001
						Flow-by	< .001
						Interaction	< .001
PSV 12 cm H ₂ O	15	2.77 (0.13)	1.65 (0.07)	2.85 (0.13)	0.57 (0.02)	Face mask	< .001
						Flow-by	< .001
						Interaction	< .001
	30	1.42 (0.06)	1.37 (0.05)	1.42 (0.06)	0.87 (0.03)	Face mask	< .001
						Flow-by	< .001
						Interaction	< .001

Measurements made during the \dot{V}_{CO_2} 300 ml/min setting.
P values determined with analysis of variance.

Amount of Rebreathing When Leaks Are Added

To test the DiMax0 mask in a scenario similar to those seen clinically, we allowed a 20% leak of the set V_T (Fig. 3). First, we recorded the effect of the leaks on rebreathing, and we found that, as expected, leaks significantly reduced rebreathing within the same mask in each ventilation setting. When comparing the 2 masks, the effect of the DiMax0 mask on rebreathing was, as expected, blunted compared to the setting without leaks. Nevertheless, the DiMax0 mask was able to significantly reduce rebreathing by 80% in CPAP with a flow of 90 L/min, by 30% in PSV at 6 cm H₂O with flow-by, and by 10% in PSV at 12 cm H₂O with flow-by, confirming the data that the addition of flow-by greatly enhanced the effectiveness of the DiMax0 mask. Figure 3 shows the results obtained with the simulated breathing frequency set at 30 breaths/min. The experiment performed with the simulated breathing frequency set at 15 breaths/min is shown in the online data supplement (see the supplementary materials at <http://www.rcjournal.com>).

Discussion

The main result of this study can be summarized as follows: separate ports for inflow and outflow substan-

tially reduced rebreathing in a total face mask, especially during CPAP and PSV with flow-by and no leaks.

In this bench study, we found that the amount of CO₂ inhaled at every breath can be as high as 6% of the \dot{V}_{CO_2} (about 18 mL for a \dot{V}_{CO_2} of 300 mL), an amount almost double the results reported by Schettino et al²³ when using a total face mask (10.4 mL/breath). This may be clinically relevant, particularly in patients with high ventilation demand and limited muscle reserve, and this likely contributes to the high incidence of NIV failure reported in more severe patients. Of relevance, rebreathing is not only an issue in hypercapnic patients, but also in hypoxemic patients, who normally exhibit a high respiratory drive and a normal/low P_{aCO_2} ²⁵; in these patients, rebreathing would represent an adjunctive ventilatory stimulus, further increasing respiratory drive and minute ventilation.

As stated, the separation of the inflow and outflow ports allowed a significant reduction in the amount of rebreathing. With a standard mask design, the air flow bypasses the volume of the entire mask (flowing around the Y-piece of the ventilator circuit), while with the separate port design, fresh air flow is forced into the mask dead space. This phenomenon is attenuated by higher breathing frequencies that reduce expiratory time, during which CO₂ washout occurs.

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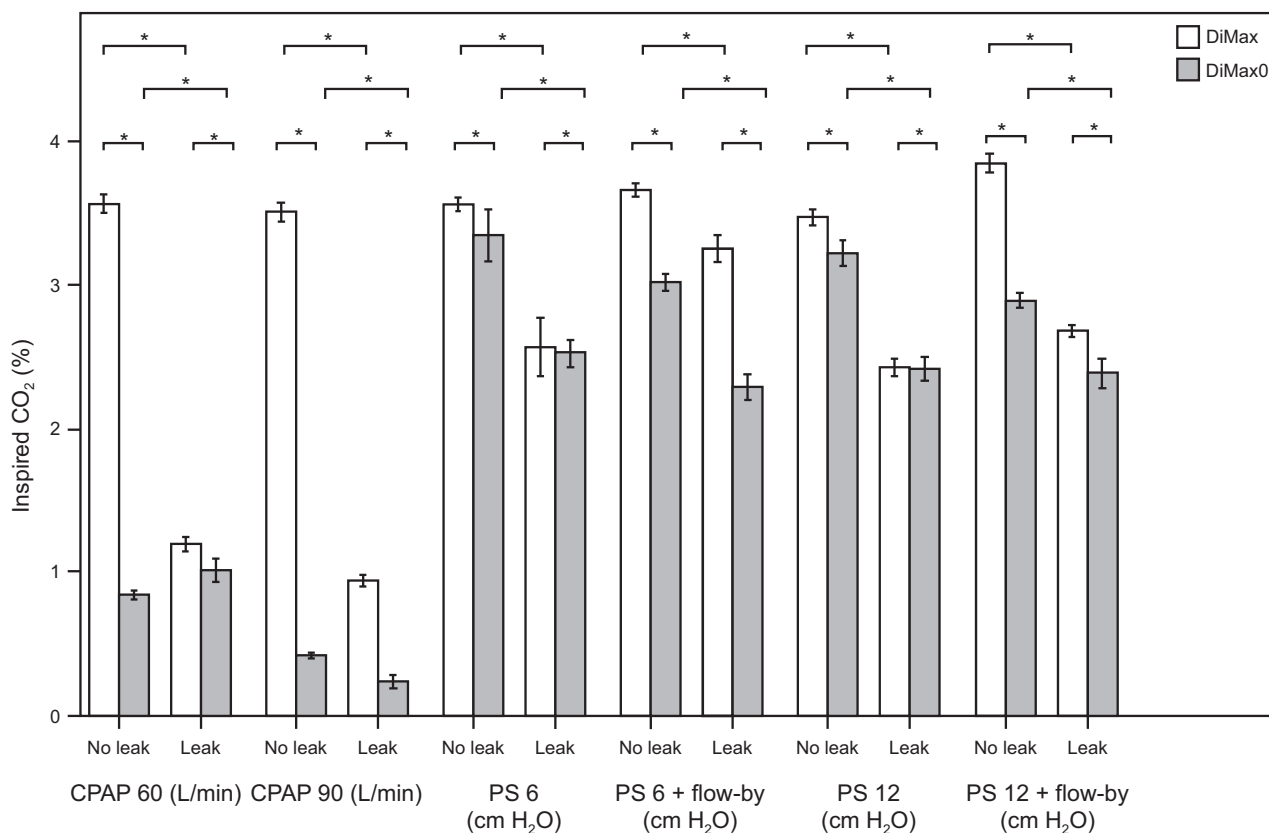


Fig. 3. Inspired CO₂ per breath, expressed as % of \dot{V}_{CO_2} , with simulated breathing frequency set at 30 breaths/min, after adding a 20% leak on tidal volume ($\dot{V}_{CO_2} = 300$ mL/min). Error bars indicate SD. PS = pressure support. ANOVA results: $P < .001$ for face-mask effect and for air-leak effect, interaction $P < .001$ in each ventilation condition. * $P < .001$.

To obtain significant CO₂ clearance from the mask, even with a separate port design, an adequate amount of fresh gas must flow through the system; the advantage is almost negligible at the lowest bias flows (2 L/min), but it becomes evident when this is increased to the highest flow allowed by the ventilator (15 L/min of fresh gas flow). Finally, the high flows during CPAP (60–90 L/min of fresh gas flow) allow an adequate CO₂ clearance even at higher breathing frequencies. Because not all mechanical ventilators allow an arbitrary increase in flow-by settings, the clinical applicability of these findings might be limited depending on the specific devices available at each center.

Each system for NIV also affects a patient's work load, which we estimated as the pressure drop during inspiration. During CPAP, this indicates that the set flow was not enough to maintain stable PEEP while inspiration was starting, whereas during PSV, the reduction in inspiratory pressure is the trigger for the ventilator to deliver the set pressure support. The 2 masks in this study showed slightly different pneumatic performances, without a consistent difference one way or another. Moreover, although statistically significant due to the lack of variability (as expected in a bench setting), the differences were modest and likely

are not clinically relevant. For this reason, we consider the masks equivalent from this perspective.

Due to the specific type of ventilator used, the application of a higher flow-by also affected the triggering sensitivity. Hence, despite a better CO₂ washout, higher flow-by resulted in a greater pressure drop during inspiration. This problem can be solved easily with the use of ventilators that allow the operator to set flow-by and trigger sensitivity independently.

Leaks (whether intentional or unintentional) are often advocated as a workaround to decrease rebreathing because these ultimately increase the fresh gas flowing through the mask. We confirm this knowledge, but our results also show that, as opposed to continuous-flow CPAP, the efficacy of leaks during PSV is limited because the ventilator will deliver additional gas flow only to compensate for the leaks. This means that the gas leaving the face mask through the leaks will ultimately be lower. Moreover, during PSV leaks might worsen patient-ventilator synchrony, possibly offsetting some of the advantages of the improved CO₂ clearance. As a side result, our study also suggests effective ways to reduce rebreathing during a CPAP or NIV trial while using the interfaces already

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available on the market: a higher flow should be used during CPAP, and a ventilator that allows a high flow-by setting should be chosen to deliver NIV.

In this study, we attempted to simulate different types of ventilatory assistance: first we simulated CPAP with a “moderate” PEEP level of 8 cm H₂O, which could be used in a patient with obstructive apnea or mild hypoxia. Then we tested 2 different levels of support: 6 cm H₂O and 12 cm H₂O, as one would use for increasing levels of respiratory distress, with a modest PEEP of 4 cm H₂O to avoid an unrealistically high peak inspiratory pressure. We also simulated 2 extreme breathing frequencies, leading to different minute ventilations and peak inspiratory flows, finding consistent results in all of the different combinations.

Although promising, the results of this bench study do not allow us to draw definitive conclusions on the effect that this modified face mask design could have on a patient’s breathing effort, NIV efficacy, and ultimate clinical outcomes. Clinical studies are needed to confirm the relevance of these findings. If confirmed, the implementation of a NIV application with this new mask could be cost-effective. The novel mask has the same cost as the standard mask from the same manufacturer. In addition, reducing rebreathing will ultimately lead to a higher rate of NIV success and less intubation, with an overall advantage for both patients and hospital costs.

Conclusion

The delivery of NIV, during both continuous-flow CPAP and PSV, is associated with clinically relevant rebreathing, which is decreased by the presence of leaks. Rebreathing can be mitigated by a face mask design with separate ports for inflow and outflow; this design is effective if a sufficient amount of additional flow-by is provided by a continuous-flow system or by the mechanical ventilator.

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