Humidification in Very-High-Flow Nasal-Cannula Therapy in an Adult Lung Model

Yusuke Chikata, Keisuke Morinishi, and Masaji Nishimura

BACKGROUND: High-flow nasal cannula (HFNC) therapy is used for patients with respiratory failure. Recently, HFNC therapy with very high gas flows (ie, gas flows of 60-100 L/min) was reported to generate higher positive airway pressure and an associated decrease in breathing frequency. However, the humidification of HFNC therapy with very high gas flow remains to be clarified. METHODS: We evaluated 3 heated humidifier systems: a single MR850, the Hummax2, and parallel MR850s. The MR850 is a pass-over humidifier system, and the Hummax2 works with a porous hollow polyethylene fiber membrane. The parallel MR850 system included 2 MR850s connected in parallel to the lung with a 22 mm Y-piece. Gas flow was set at 40–90 L/min in increments of 10 L/min, and $F_{\rm IO_2}$ was set at 0.21. Heated humidifiers in the MR850 systems were set in invasive mode (40°C/ $^{-}$ 3), and with the Hummax2 the vapor temperature was set at 39°C. The simulated external nares were connected to a test lung via a standard ventilator circuit. One-way valves prevented mixing of inspired and expired gases. Compliance of the test lung was 0.05 L/cm H₂O and resistance 5 cm H₂O/L/s. Simulated tidal volumes (V_T) were 300, 500, and 700 mL, with a breathing frequency of 10 or 20 breaths/min and an inspiratory time of 1.0 s. Temperature, relative humidity, and absolute humidity (AH) of inspired gas downstream of the external nares were measured using a hygrometer for 1 min, and results for the last 3 breaths were extracted. RESULTS: With the single MR850, when gas flow was > 80 L/min, AH decreased as gas flow increased (P < .001). With the Hummax2, as gas flow increased, AH decreased (P < .001). With the parallel MR850s, regardless of gas flow, AH was constant. As breathing frequency increased, AH increased in all systems. CONCLUSIONS: During HFNC therapy with very high gas flows in this bench study, conventional heated humidifiers did not provide adequate humidification. Caution is advised when using HFNC therapy with very high gas flows with conventional heated humidifiers. Key words: humidification; heated humidifier; very high flow gas. [Respir Care 2019;64(7):809–817. © 2019 Daedalus Enterprises]

Introduction

When acute hypoxemic respiratory failure occurs, oxygen therapy is the first line of intervention, and high-flow nasal cannula (HFNC) therapy is now commonly administered to patients with acute respiratory failure. Delivering up to 60 L/min of heated and humidified medical gas via a wide-bore nasal cannula, HFNC therapy has a num-

ber of physiological benefits, including washout of carbon dioxide in nasopharyngeal dead space, adequate humidification, accurate maintenance of $F_{\rm IO_2}$, low PEEP level, and reduced respiratory effort.

Recently, with a report showing that flows of up to 100 L/min result in increased pharyngeal airway pressure of 1 cm H₂O per 10 L/min of flow, HFNC therapy with very high gas flows (ie, gas flow of 60–100 L/min) has

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The authors have disclosed no conflicts of interest.

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been shown to have a greater beneficial effect: as gas flow increases, breathing frequency decreases.⁸ There are few reports of the impact of HFNC therapy with very high gas flows. To deliver constant flow by using wall pressure supply, 60–70 L/min is maximal; however, there are no adequate flow meters for flows > 60 L/min.

The performance of a heated humidifier is affected by gas flow and environmental conditions.^{3,9,10} In a previous bench study using an adult lung model, under various respiratory parameters and different gas flows, we evaluated the humidification performance of a heated humidifier with HFNC therapy.^{3,10} In this study, we evaluated the adequacy of humidification during conventional HFNC therapy (ie, gas flow of 40–50 L/min) and HFNC therapy with very high gas flows (ie, gas flow of 60–90 L/min).

Methods

Tested HFNC Systems

We evaluated 3 heated humidifier systems, the MR850 (Fisher & Paykel, Auckland, New Zealand), the Hummax2 (Metran, Saitama, Japan), and 2 MR850 systems set up in parallel. The MR850 passes gas directly over exposed heating wires; in the Hummax2, gas flows through a hollow porous polyethylene fiber membrane inside the respiratory circuit. The MR850 has an auto-active compensatory algorithm that continuously monitors gas flow and the temperature of the chamber outlet and the distal temperature probe, adjusting the temperature to prevent excessive condensation. The Hummax2 is only able to set the vapor temperature between 32°C and 39°C. The parallel MR850 systems included a 22-mm Y-piece that joined flow delivery (see Fig. 1, Fig. 2).

Each humidifier system was set up between the wall gas supply with gas flow through an air/oxygen blender with a very-high-flow regulator (10–90 L/min, OA2080, San-You Technology, Saitama, Japan) and the cannula interface with the model lung. Manufacturer standard respiratory circuits led from the heated humidifiers (MR850 via RT202, Fisher & Paykel; Hummax2 via R100-H, Metran) to nasal prongs (OPT544, Fisher & Paykel).

Simulated Spontaneous Breathing

Spontaneous breathing was simulated using a training test lung (TTL model 1601, Michigan Instruments, Grand Rapids, Michigan). After the muscle and lung compartments of the test lung were connected, the Puritan-Bennett 840 (Medtronic, Minneapolis, Minnesota) inflated the muscle compartment, whereupon the lung compartment inspired medical gas and some ambient via the HFNC. To simulate external nares, we made 2 holes in a polyvinyl

QUICK LOOK

Current knowledge

High-flow nasal cannula (HFNC) therapy is widely used for patients with respiratory failure. Normally, during HFNC therapy, gas flow is set to 30–60 L/min. One advantage of HFNC therapy over other therapies is superior humidification. Recently, HFNC therapy with very high gas flow (ie, with gas flows of 60–100 L/min) was reported to generate higher positive airway pressure and an associated decrease in breathing frequency.

What this paper contributes to our knowledge

At HFNC flows > 60 L/min, the 2 tested heated humidifier systems did not maintain the set temperature when used individually. At flows > 90 L/min, the absolute humidity delivered by the individual heated humidifiers (ie, < 30 mg/L) was inadequate. When applying HFNC with very high gas flows, it is expedient to use 2 MR850 devices connected in parallel with a Y-piece.

chloride cylinder closed at one end and connected to the lung compartment of the TTL test lung at the other end via a standard ventilator circuit (Smoothbore tube 5000000, Intersurgical, Berkshire, United Kingdom). One-way valves prevented the mixing of inspired and expired gases (Fig. 3). TTL test lung compliance was 0.05 L/cm H₂O, and resistance was 5 cm H₂O/L/s. Simulated tidal volume (V_T) was set, with decelerating flow waveform, at 300, 500, and 700 mL, with a breathing frequency of 10 or 20 breaths/min and an inspiratory time of 1.0 s. These settings resulted in 33, 55, and 77 L/min of spontaneous breathing at peak inspiratory flow. To monitor V_T delivery, gas flow to the lung compartment was measured using a pneumotachometer (4700 series, 0-160 L/min, Hans Rudolph, Shawnee, Kansas) with a differential pressure transducer (TP-602T, ± 5 cm H₂O, Nihon Kohden, Tokyo, Japan). The pneumotachometer was calibrated using a super syringe.

Experimental Procedures

Both the single MR850 system and the parallel MR850 system were set in the "invasive with auto-active compensatory mode" (40°C/–3); in the Hummax2 system, vapor temperature was set at 39°C. With the single MR850 and the Hummax2, gas flow was set at 40–90 L/min in increments of 10 L/min, and $F_{\rm IO_2}$ was set at 0.21. With the parallel MR850 system, the gas flow was divided equally between both devices.

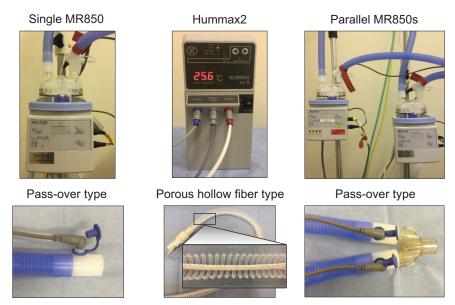


Fig. 1. Tested heated humidifiers. The single MR850 was evaluated as conventional HFNC system, The Hummax2 is a type of porous hollow fiber membrane, it generates vapor in set temperature. The parallel MR850s were used as two gas blenders and heated humidifiers and both tubes were connected in parallel with a 22 mm Y-piece.

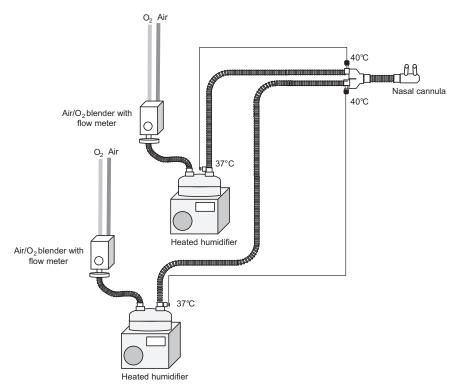


Fig. 2. The parallel MR850 system incorporated two O_2 /air blenders with high-flow meter (0-60 L/min), two heated humidifiers, two manufacturer standard circuits and a nasal prong. Outlets of each circuit were connected with a 22 mm Y-piece for joint delivery of the HFNC. The set up of the other two systems was similar, but without the inclusion of a second humidifier and circuit or Y-piece. The temperatures are as set for each MR850.

Before experimental testing, a ventilator self-test was performed. After each experimental setting was changed, we allowed at least 15 min for stabilization. Temperature,

relative humidity, and absolute humidity (AH) of inspired gas immediately downstream from the external nares were measured using a hygrometer (Moiscope, Senko Medical,

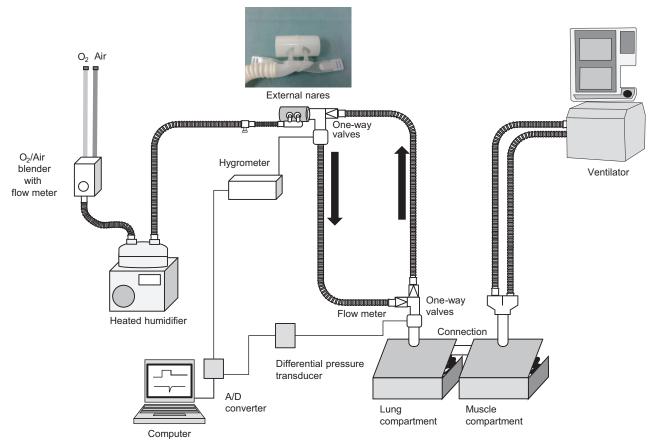


Fig. 3. Spontaneous breathing was simulated using a mechanical ventilator and TTL test lung. To simulate spontaneous breathing, the muscle and lung compartment of the test lung were connected so that the ventilator inflated the muscle compartment, causing the lung compartment to inspire HFNC medical gas and ambient air. One-way valves prevented mixing of inspired and expired gases. During simulated inspiration, medical gas and ambient air are drawn into the lung compartment past the hygrometer. We made two holes in polyvinyl chloride cylinder to simulate external nares. The external nares were connected to the lung compartment of TTL test lung via a standard ventilator circuit. To confirm tidal volume delivered to the lung compartment, flow to the lung compartment was measured using a pneumotachometer with a differential pressure transducer.

Tokyo, Japan) for 1 min, and the results for the last 3 breaths were extracted. The thermometer was calibrated using a cooler/heater water source (HHC-51, Senko Medical). All signals were processed through an analog/digital converter and saved on a computer at 50 Hz/channel using data acquisition software (WinDaq, Dataq Instruments, Akron, Ohio). The results were expressed as median and IQRs. All experiments were performed in an air-conditioned room where temperature was maintained at 24°C, and ambient temperature and AH were monitored.

Statistics

Repeated measures of analysis of variance were performed. All statistical tests were 2-sided, and P values < .05 were considered statistically significant. All statistical analysis was performed using commercial software (SPSS 11.01, SPSS, Chicago, Illinois).

Results

Throughout the protocols, ambient AH was 4.6 ± 2.0 mg/L, and temperature was 24.1 ± 0.2 °C. During simulated spontaneous breathing, V_T was measured as 278 ± 9.5 , 488 ± 7.5 , and 682 ± 9.2 mL when set V_T was 300, 500, and 700 mL, respectively.

Effect of Very-High Gas Flow on AH

At very-high gas flow of 40–90 L/min, increasing in increments of 10 L/min, respective AH readings with the single MR850 system were 33.4 mg/mL (32.6–34.7), 34.0 mg/mL (32.7–36.0), 35.7 mg/mL (34.1–36.7), 35.4 mg/mL (34.3–36.5), 31.5 mg/mL (30.1–33.5), and 29.6 mg/mL (28.8–31.1); with the Hummax2 system, the respective AH readings were 34.3 mg/mL (33.1–35.9), 33.6 mg/mL (32.5–35.6), 32.1 mg/mL (31.3–33.5), 29.5 mg/mL (28.0–30.5), 27.8 mg/mL (27.0–28.5), and

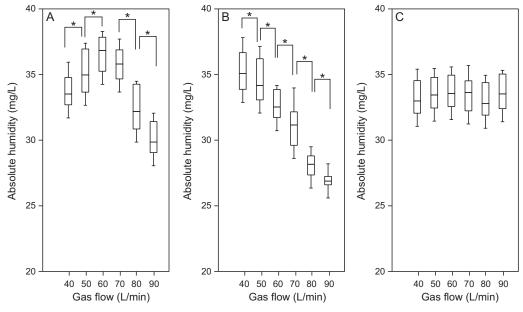


Fig. 4. With the single MR850 (A), at HFNC gas flow 40-60 L/min at each 10 L/min increment, absolute humidity increased. At HFNC gas flow increments above 80 L/min, however, absolute humidity decreased. With the Hummax2 (B), as HFNC gas flow increased, absolute humidity decreased. With the parallel MR850s (C), absolute humidity was constant regardless of HFNC gas flow. * P < .05.

26.9 mg/mL (26.6–27.2); with the parallel MR850 system, respective AH readings were 32.8 mg/mL (31.9–34.4), 33.0 mg/mL (32.0–34.4), 33.0 mg/mL (32.0–34.4), 32.8 mg/mL (31.4–33.7), 32.5 mg/mL (31.7–34.1), and 32.9 mg/mL (31.8–34.4). With the single MR850 system, as gas flow increased in increments of 10 L/min from 40-60 L/min, AH remained constant. At flows above 80 L/min, however, AH decreased (P < .001). With the Hummax2 system, as flow increased, AH decreased (P < .001). With the parallel MR850 system, AH remained constant regardless of gas flow (Fig. 4).

Effect of V_T on AH

With the single MR850 system, at very-high gas flows of 40, 50, and 60 L/min, as V_T increased, AH increased. When the gas flow was > 70 L/min, AH remained the same when V_T was 500 and 700 mL. With the Hummax2 system, at gas flows of 40 and 50 L/min, as V_T increased, AH increased; at gas flows 60-80 L/min, when V_T changed from 500 to 700 mL, AH was affected by V_T ; at a flow of 90 L/min, however, AH was not affected by variations in V_T . With the parallel MR850 system, as V_T increased, AH increased (Table 1, Fig. 5).

Effect of Breathing Frequency on AH

With each of the tested systems, as breathing frequency increased, AH increased (P < .001) (Fig. 6).

Discussion

In this study, we tested various simulated spontaneous breathing patterns to investigate how well 3 types of heated humidifiers maintained humidification during HFNC therapy with very high gas flow. When flow was >70 L/min, neither the single MR850 system nor the Hummax2 system maintained AH at 30 mg/L. At flows of up to 90 L/min, the parallel MR850 system consistently maintained AH at > 30 mg/L.

Effect of HFNC Gas Flow on AH

Chikata et al³ conducted bench-study evaluations of humidification performance during HFNC therapy, and they found that AH values with an MR850 were 33.1 ± 1.5 mg/mL, 35.9 ± 1.7 mg/mL, and 36.2 ± 1.7 mg/L at gas flows of 20, 40, and 50 L/min, respectively. Internal condensation varied according to ambient temperature; the lower the temperature, the greater the volume of condensate. In our study, AH was lower at gas flows of 40 and 50 L/min than in their study, possibly due to the higher ambient temperature in ths study $(25.6 \pm 0.5^{\circ}\text{C})$ vs $24.1 \pm 0.2^{\circ}\text{C}$.

With the single MR850 system, as very-high gas flow increased, AH increased, and at gas flows > 80 L/min, AH decreased. Chikata et al³ reported that as gas flow increased, the AH of inspired gas increased. At gas flows of 60 L/min or more, the electrical output of the humidifier heater plates was continuously 100% and the

Effect of V_T and Gas Flow on Absolute Humidity

HFNC System	Flow (L/min)	Absolute Humidity, mg/L		
		$V_T = 300 \text{ mL}$	$V_T = 500 \text{ mL}$	$V_T = 700 \text{ mL}$
Single MR850	40	32.6 (31.4–33.8)	33.6 (32.6–34.7)	33.7 (32.8–35.5)
	50	33.1 (31.9–34.4)	34.4 (32.7–36.3)	34.9 (33.7-36.4)
	60	34.2 (32.5–36.0)	35.4 (34.1–36.7)	35.9 (35.6-36.9)
	70	35.3 (33.3–36.2)	35.4 (34.3–36.5)	35.4 (35.2–36.8)
	80	30.4 (28.8–32.0)	32.0 (30.3–33.5)	31.5 (31.3-33.2)
	90	28.9 (27.8–30.1)	29.9 (28.8–31.1)	30.1 (29.1-31.2)
Hummax2	40	33.6 (32.5–34.5)	34.6 (33.1–35.9)	35.5 (34.0-37.0)
	50	33.4 (32.5–34.0)	33.7 (31.7–35.6)	34.9 (33.2-36.6)
	60	32.0 (31.3–32.4)	31.7 (29.9–33.5)	32.8 (31.8-33.8)
	70	28.4 (27.3–29.4)	28.9 (28.0–29.7)	31.5 (30.6-32.4)
	80	27.7 (27.0–28.5)	27.6 (26.9–28.3)	28.3 (27.5-29.2)
	90	26.9 (26.7–27.2)	26.9 (26.6–27.0)	26.7 (25.0-28.2)
Parallel MR850	40	32.0 (30.5–33.5)	33.2 (32.0-34.4)	33.7 (32.1-35.2)
	50	32.8 (32.0–33.6)	33.2 (32.0–34.4)	33.8 (32.5-35.0)
	60	32.2 (31.2–33.3)	33.2 (32.0-34.4)	33.8 (32.7-35.0)
	70	32.0 (30.8–33.2)	32.6 (31.4–33.7)	33.4 (32.3-34.8)
	80	32.1 (31.0–33.3)	32.9 (31.7–34.1)	33.3 (31.9-34.7)
	90	32.0 (30.8–33.3)	33.2 (31.8–34.4)	33.7 (32.5-34.7)

V_T = tidal volume

humidifier-outlet and tube-end temperatures were lower than set, a limit that restricted the amount of vapor the MR850 could deliver¹⁰; consequently, as gas flow increased, AH decreased. With the Hummax2, at each increment, as very-high gas flow increased, AH decreased. With the single MR850 and the Hummax2 systems, at gas flows > 60 L/min, temperature was unstable (Fig. 7); fluctuations were more pronounced with the Hummax2 than with the single MR850. By contrast, in the parallel MR850 system, temperature remained stable. The Hummax2 uses a porous hollow polyethylene fiber membrane, and the temperature is servo-controlled by sensing temperature only at the distal end of the tube away from the water reservoir; the system design delivered less vapor in our test protocols. With the parallel MR850 system, during HFNC therapy, maximum gas flow through each heated humidifier was 45 L/min. At gas flows of 40 L/min or less, the temperature at the outlet of the water reservoir and at the end of the inspiratory tube remained at the set temperature, and the electrical output of the heated humidifier heater plates was < 100%.

Effect of V_T and Breathing Frequency on AH

With the single MR850 system, at very-high gas flows of 40, 50 and 60 L/min, as V_T increased, AH increased. When gas flow increased to > 70 L/min, the effect on AH

was negligible when V_T varied between 500 and 700 mL. With the Hummax2, at very-high gas flows of 40 and 50 L/min, as V_T increased, AH increased. As shown in Figure 4, as V_T increased, these 2 systems were unable to maintain the desired levels of AH at higher levels of gas flow; the Humamx2 performed inconsistently at HFNC flows > 60 L/min, and the single MR850 performed inconsistently at levels > 80 L/min. By contrast, regardless of V_T setting, the parallel MR850 system reliably delivered adequate AH.

Humidity during HFNC therapy depends on both inspiratory flow of spontaneous breathing and gas flow. When spontaneous breathing inspiratory flow is less than the gas flow, in theory, patients would inspire only the gas delivered via the cannula, and thus, due to the high flow, adequate humidification of the gas reaching the lungs would depend on adequate humidification of the delivered gas. On the other hand, when the inspiratory flow of spontaneous breathing is greater than the gas flow, patients inspire a mixture of delivered gas and room air. When V_T was set at 300, 500, and 700 mL, and inspiratory time was set at 1.0 s with a decelerating flow waveform, peak inspiratory flows of spontaneous breathing were 33, 55, and 77 L/min, respectively. Consequently, at each V_T setting, when gas flow is > 80 L/min, patients would, in theory, inhale only gas. In spontaneous breathing, inspiratory gas is normally heated and humidified in the nasal cavity and pharynx. Due to the higher gas flow during HFNC ther-

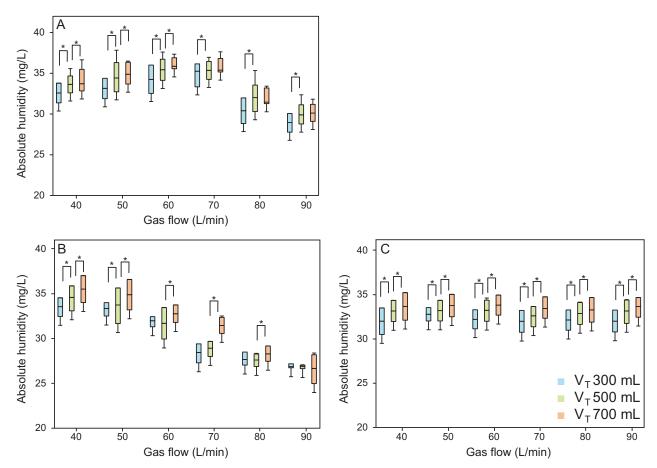


Fig. 5. With the single MR850, at HFNC gas flow of 40, 50 and 60 L/min, as V_T increased, AH increased. At HFNC gas flows greater than 70 L/min, when V_T varied between 500 to 700 mL, AH was not affected. With the Hummax2, at HFNC gas flow 40 and 50 L/min, as V_T increased, AH increased. At flow of 60–80 L/min, when increased to 700 mL, V_T affected AH. With the parallel MR850s, as V_T increased, AH increased at all HFNC gas flow settings.

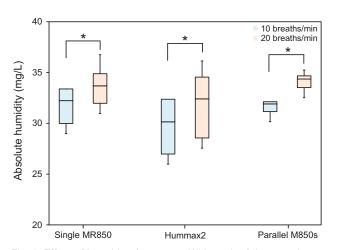


Fig. 6. Effect of breathing frequency. With each of the tested systems, as breathing frequency increased, absolute humidity increased.

apy, humidification performance is much more heavily dependent on the humidity of the inspired gas and room air. Although we made the distance between the external nares and hygrometer as short as we could, it is likely that inspired gas temperature was affected by ambient air temperature. In addition, as V_T at a fixed inspiratory time of 1.0 s increased, inspiratory flow increased. Because the inspiratory flow of simulated spontaneous breathing is more rapid, gas at HFNC flow levels remains in the simulated nasal cavity and pharynx for less time, and, consequently, the medical gas is less cooled. With the single MR850 system and the Hummax2, at very-high gas flows (ie, > 60 L/min), the servo-control of the heated humidifier was unreliable. As a result, the 2 single-humidifier systems showed inconsistencies at higher levels of gas flow

As breathing frequency increased, AH increased, and the time between breaths decreased. Therefore, there are few effects of environmental temperature in this bench study.

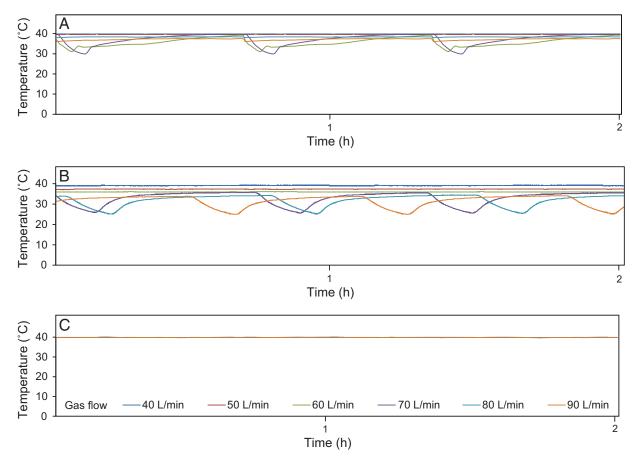


Fig. 7. Temperature at tube end in each system. Distal temperature in tubes was measured for 60 min in each device at each high-flow gas flow setting. A: Single MR850 set at 40°C, B: Hummax2 set at 39°C, and C: parallel MR850s set at 40°C. With both single humidifier systems, at HFNC gas flows greater than 60 L/min, the temperature was not stable. Both the frequency and degree of inconsistency was greater with the Hummax2 than with the single MR850. With the parallel MR850s, temperature remained stable.

Limitations

Aside from being a bench study, the findings of which cannot be directly applied to clinical settings, our experiment has some limitations. First, our study used a closed-mouth simulation. Real patients, if breathing through the mouth, would inspire more ambient air. In addition, actual human V_T varies and, in real lungs, actual AH might vary breath-by-breath.¹¹ Second, the study was done using only one inspiratory flow waveform; in real life, peak inspiratory flow varies from patient to patient and from breath to breath. The V_T of patients with respiratory failure is greater than the V_T settings we tested. Finally, we had difficulty simulating a comprised oropharynx and the dead space associated with such compromise.

Conclusions

Using a lung model and various respiratory patterns, we evaluated the humidification performance of 3 heated humidifier systems during HFNC with very high gas flow. At

gas flows > 60 L/min, the 2 single-humidifier systems we tested were unable to reliably maintain the set temperature. However, 2 MR850 devices set up in parallel were able to maintain set temperature in all gas flow settings. When using the O_2 /air blenders at very high flows for patients, we recommend using parallel heated humidifiers and carefully observing vital signs and sputum characteristics.

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SIMULATED HUMIDIFICATION IN VERY-HIGH-FLOW NASAL CANNULA

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